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1 ORIGINAL RESEARCH ARTICLE

2
3 **Title:**

4 To walk or to run – a question of movement attractor stability

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26 **Running title:**

27 Gait mode and movement attractor stability

28 **Key words:**

29 Locomotion, attractor stability, dynamics, coordination, gait

30

31 **Summary statement**

32 The present study shows in accordance with the Dynamical Systems Theory, that lower
33 limb attractor stability is highest at a particular gait mode closest to the corresponding preferred
34 speed.

35

36 **Abstract**

37 During locomotion, humans change gait mode between walking and running as
38 locomotion speed is either increased or decreased. Dynamical Systems Theory predicts that the
39 self-organization of coordinated motor behaviors dictates the transition from one distinct stable
40 attractor behavior to another distinct attractor behavior (e.g. walk to run or vice versa) as the
41 speed is changed. To evaluate this prediction, the present study investigated the attractor stability
42 of walking and running across a range of speeds evoking both self-selected gait mode and non-
43 self-selected gait mode. Eleven subjects completed treadmill walking for 3 minutes at 0.89, 1.12,
44 1.34, 1.56, 1.79, 2.01, 2.24, 2.46 m/s and running for 3 minutes at 1.79, 2.01, 2.24, 2.46, 2.68,
45 2.91, 3.13, 3.35 m/s in randomized order while lower limb joint angles and sacrum
46 displacements was recorded. Attractor stability was quantified by continuous relative phase and
47 deviation phase of lower limb segment angles, and the largest Lyapunov exponent, correlation
48 dimension and movement variability of the sacrum marker displacement and the hip, knee and
49 ankle joint angles. Lower limb attractor stability during walking was maximized at speeds close
50 to the self-selected preferred walking speed and increased during running as speed was
51 increased. Furthermore, lower limb attractor stability was highest at a particular gait mode
52 closest to the corresponding preferred speed, in support of the prediction of Dynamical Systems
53 Theory. This was not the case for the sacrum displacement attractor, suggesting that lower limb
54 attractor behavior provides a more appropriate order parameter compared to sacrum
55 displacement.

56

57 **1. Introduction**

58 **1.1 Gait mode selection**

59 During terrestrial locomotion, bipeds and quadrupeds are able to shift between multiple
60 gait modes, with the transition occurring within a relatively few steps (e.g. from walk to run or
61 trot to gallop). The underlying control mechanisms that evoke the transition between gait modes
62 have been investigated intensively, and several possible driving factors have been discussed in
63 the literature. These involve the minimization of energy expenditure (Hoyt and Taylor, 1981;
64 Hreljac, 1993b; Minetti et al., 1994; Thorstensson and Roberthson, 1987), the mechanical
65 limitation of different gait modes (Alexander, 1977; Hreljac, 1993a; Hreljac, 1995a; Hreljac,
66 1995b; Kram et al., 1997; Ranisavljev et al., 2014; Thorstensson and Roberthson, 1987), the
67 minimization of mechanical stress (Biewener and Taylor, 1986; Biewener et al., 1983; Farley
68 and Taylor, 1991; Hreljac, 1993a; Taylor, 1985) and the integration of sensory input and
69 centrally controlled rhythmic motor output (Caggiano et al., 2018; Hansen et al., 2017; Kiehn,
70 2016; Prilutsky and Gregor, 2001; Thorstensson and Roberthson, 1987; Voigt et al., 2019).

71 These explanations primarily focus on a minimization or optimization of a specific
72 parameter that constitutes the governing mechanism for the transition between gait modes. This
73 suggests that comprehensive computational work is required to determine when it is beneficial to
74 change gait. It also implies that a cost function (e.g. related to energy expenditure, muscular
75 stress or joint forces) dictates the executed movements. However, as an alternative to this,
76 Dynamical Systems Theory suggests that the executed movement originates from a self-
77 organization process creating better coordinated motor behaviors (i.e. the best solution given the
78 constraints on the system and the task at hand) (Kelso et al., 1979). Furthermore, changes in
79 motor behavior occur through phase transition from one stable attractor behavior to another (e.g.
80 walk to run) (Haken et al., 1985; Kelso and Schöner, 1988). These changes can be initiated by
81 alterations in a control parameter (e.g. movement frequency or speed). The behavior of the
82 attractor can be summarized by an order parameter, i.e. a low-dimensional collective variable
83 providing a measure of the organizational state of the system (Haken, 1983).

84 In their seminal work, Diedrich and Warren (Diedrich and Warren, 1998; Diedrich and
85 Warren, 1995) presented an illustration of the phase transition between two attractors in relation
86 to human locomotion. This transition includes: 1) a qualitative change in the order parameter, 2)
87 a sudden jump in the order parameter as the control parameter is continuously changed, 3) a

88 resistance to change to another basin of attraction as the control parameter is changed and 4)
89 decreased attractor stability, indicated by an increase in the magnitude of the variability of the
90 order parameter when approaching the transition point. Hence, two different principles can be
91 inferred. First, a *control parameter-dependent attractor stability principle* would suggest that a
92 change in control parameter (in this case, locomotion speed) will move the system from one
93 stable attractor (i.e. walking at the preferred walking speed (PWS)) through an unstable region
94 before abruptly switching to a different, stable attractor (i.e. running at the preferred running
95 speed (PRS)). Secondly, an *attractor stability optimization principle* would suggest that the self-
96 selected movement solution at a given speed will exhibit a more stable attractor compared to the
97 alternative movement solution. This means that walking at speeds close to PWS will exhibit a
98 more stable attractor compared to running at the same speed. Similarly, running at speeds close
99 to the PRS will exhibit a more stable attractor compared to walking at the same speed. To test
100 these two inferred principles experimentally, Diedrich and Warren (1995) recruited healthy
101 individuals to both walk and run at speeds ranging from below to above the walk-to-run
102 transition speed. The attractor stability was quantified as the variation in the relative phase of the
103 intersegmental lower limb coordination (i.e. the coupling between lower limb joint angles within
104 the same leg (Diedrich and Warren, 1995)). In support of the two inferred principles, it was
105 observed that the stability decreased during walking at both low and high walking speeds with a
106 local maximum at intermediate speeds close to PWS, and the stability decreased at low running
107 speeds but increased or remained constant at high running speeds. Furthermore, it was observed
108 that stability was higher during walking at relatively low speeds compared to running at the same
109 speed. The opposite pattern was seen at relatively high speeds but only for the ankle-knee joint
110 coupling (Diedrich and Warren, 1995).

111 **1.2 Dynamics of human locomotion**

112 The method applied by Diedrich and Warren (Diedrich and Warren, 1998; Diedrich and
113 Warren, 1995) captures the spatiotemporal configurations of the system by providing a measure
114 of the synchronized oscillatory motion of two coupled segments. However, according to
115 Dynamical Systems Theory the attractor behavior of the system in question is characterized not
116 only by the spatiotemporal configurations of elements (e.g. coordination of segments across the
117 gait cycle) but also by the temporal development of the spatial configurations, i.e. the dynamics.
118 The latter part addresses how one spatial configuration influences future configurations (e.g. the

119 temporal relationship between subsequent coordination of segments) and has been linked to the
120 underlying motor control strategy (Newell and Corcos, 1993). This feature of dynamical systems
121 is related to the attractor stability (Stergiou, 2004; Stergiou, 2016). Thus, increased attractor
122 stability of a dynamical system is characterized by a high statistical likelihood of the
123 reoccurrence of specific patterns in specific orders whereas decreased attractor stability is
124 characterized by a random structure with low statistical likelihood of repeated patterns.
125 Therefore, we argue that the investigation of stability according to Diedrich and Warren
126 (Diedrich and Warren, 1998; Diedrich and Warren, 1995) is limited. We submit that their
127 methodology of evaluating the attractor's stability through the examination of the variation in the
128 relative phase of the intersegmental lower limb coordination needs to be supplemented with the
129 investigation of the temporal dynamics of the interacting components. Considering these
130 limitations in the investigative approach used by Diedrich and Warren (1995), it is crucial first to
131 verify their observations using a similar protocol and analytical approach and second, to confirm
132 that their conclusions hold true when the temporal dynamics is evaluated.

133 Previous studies have quantified the dynamics in continuous human movements such as
134 walking in order to investigate the underlying motor control strategy (e.g. (Chien et al., 2015;
135 England and Granata, 2007; Raffalt et al., 2017)). In agreement with the aforementioned
136 principle about control parameter-dependent attractor stability, the presence of a U-shaped
137 relationship between movement dynamics and speed has been observed for both walking (Chien
138 et al., 2015; Raffalt et al., 2017) and running (Jordan et al., 2006). However, the methodological
139 design of these studies did not challenge this attractor stability optimization principle. To do so
140 requires a study protocol that forces the motor control system to solve the locomotion task using
141 an alternative solution compared to the preferred one. Therefore, the present study included a
142 protocol similar to that of Diedrich and Warren (1995), in which the constraints of the locomotor
143 task are manipulated and the control parameter are scaled, in order to evoke both stable self-
144 selected movement solutions and unstable non-self-selected solutions to the same task. By
145 quantifying the dynamics of these alternative solutions, this alternative protocol permits the
146 attractor stability optimization principle to be challenged in the context of human locomotion.
147 The attractor stability principle optimization would be disproved if the self-selected movement
148 solution at a given speed does not exhibit greater attractor stability compared to the alternative
149 movement solution.

1.3 Order parameter identification

When assessing attractor behavior, the identification of an appropriate order parameter is crucial, and a variety of variables have been investigated in relation to human walking and running. These variables include center of mass displacement (Dingwell and Marin, 2006) or acceleration (Raffalt et al., 2017), lower limb joint angles (England and Granata, 2007; Raffalt et al., 2017) and segment angles (Diedrich and Warren, 1995; Kurz et al., 2005; Stergiou et al., 2001). The attractor behavior of center of mass variables (displacement and acceleration) represents the combined influence of all the movements within the system and can be strongly linked to the energy cost of locomotion (Gottschall and Kram, 2003; Grabowski, 2010). In contrast, the attractor behavior of the joint or segment angles originates from the oscillatory movement of the lower limb, and is related to its pendulum-like function during walking and its spring-like function during running (Cavagna and Margaria, 1966; Cavagna et al., 1963). However, to the best of our knowledge, no consensus exists on the selection of an order parameter for human locomotion. By including both center of mass variables and lower limb joint angle-based behavior attractors, the present study sought to clarify which of these variables best captures the movement dynamics of human locomotion.

1.4 Study purpose

The purpose of the present study was to investigate the attractor stability of two tasks, walking and running, across speeds, with changed task constraints evoking both stable self-selected movement solutions and unstable non-self-selected movement solutions. To fulfill this purpose, the present study adopted the same experimental and analytical approach as Diedrich and Warren (1995) and, additionally, investigated the stability of the movement attractor through an evaluation of the temporal dynamics. Furthermore, the present study aimed to identify an appropriate order parameter; investigating the response both of center of mass variables and lower limb joint angle variables to alterations in speed and task constraints. The present study included healthy young subjects who walked and ran at speeds below and above their PWS and the PRS. Continuous relative phase was used to quantify the oscillatory motion of the coupled lower limb segments as a measure of the segmental coordination, and the deviation phase was used to assess the stability of the executed coordination pattern. The temporal dynamics of the center of mass displacements and lower limb joint angles was investigated using the largest Lyapunov exponent (LyE) and correlation dimension (CoD). LyE and CoD quantify the

181 exponential rate of divergence or convergence of the attractor's trajectory in state space (Wolf et
182 al., 1985) and the fractal dimension of the attractor in the occupied state space (Grassberger and
183 Procaccia, 1983), respectively. Additionally, movement variability was assessed by the ensemble
184 average standard deviation (meanSD) of the center of mass displacement and lower limb joint
185 angles across the gait cycle.

186 In agreement with the two principles inferred from Diedrich and Warren (1995), we
187 formulated the following hypotheses: 1) the movement solution during walking at PWS and
188 during running at PRS is a stable behavioral attractor for that particular gait mode while speeds
189 below and above would display significantly different dynamics and 2) at speeds close to the
190 preferred speed of a particular gait mode the movement solution would exhibit a more stable
191 attractor behavior compared to the alternative gait mode at the same speed. When using the
192 relative phase approach, stable attractor behavior would be characterized by a low deviation
193 phase of the thigh-shank coupling and thigh-foot coupling consistent with Diedrich and Warren
194 (1995). When assessing the dynamics of the attractor behavior, stable attractors would be
195 characterized by low values of LyE and CoD and when assessing movement variability, stable
196 attractors would be characterized by a low meanSD.

197 To evaluate whether a center of mass movement based or a joint angle based attractor
198 behavior constitutes the most appropriate order parameter for human locomotion, the present
199 study included three-dimensional kinematic measurements of the sacrum position and sagittal
200 plane hip, knee and ankle joint angles. It could be speculated that the variable(s) confirming the
201 raised hypotheses would represent the most appropriate order parameter(s).

202

203 **2. Materials and methods**

204 The present investigation included analysis of data collected in a previous study (Raffalt
205 et al., 2019). The present and previous study share the same subjects and experimental
206 equipment (motion capture system and treadmill). The present study, however, includes an
207 extended protocol and analyses of unpublished data.

208 **2.1 Subjects**

209 Five males and six females (mean \pm standard deviation age: 23.3 ± 3.9 years, body
210 height: 1.74 ± 0.10 meters and body mass: 72.1 ± 14.3 kg) were included in the present study.
211 The participants were physically active, familiar with treadmill walking and running and did not
212 report any musculoskeletal injuries or cardiovascular or neurological diseases. All participants
213 were informed of the experimental procedures before giving their written consent to participate
214 in the study. The study was approved by the Institutional Review Board of the University of
215 Nebraska Medical Center and the study was carried out in accordance with the approved
216 protocol.

217 **2.2 Experimental setup and procedure**

218 After completing a brief warm up session on a treadmill, the PWS and the PRS of each
219 participant were established using a standardized protocol explained elsewhere (Dingwell and
220 Marin, 2006). Briefly, the participants were blinded to the speed of the treadmill as it was
221 gradually increased and decreased above and below what was reported as comfortable. The
222 average of the speeds reported as comfortable were termed as PWS and PRS, respectively. The
223 mean \pm standard deviation of PWS and PRS were 1.26 ± 0.23 m/s and 2.50 ± 0.34 m/s,
224 respectively. Following a short rest, the participants were fitted with 15 retro-reflective markers
225 placed bilaterally superficial to the: 1) anterior superior iliac spines, 2) greater trochanters, 3)
226 lateral knees, 4) tibial tubercles, 5) lateral ankles, 6) posterior heels (on shoes) and 7) fifth
227 metatarsal heads, laterally (on shoes). An additional single marker was placed on the sacrum
228 (Vaughan et al., 1992). The participants then completed 8 trials of 3 minutes walking at 0.89,
229 1.12, 1.34, 1.56, 1.79, 2.01, 2.24, 2.46 m/s and 8 trials of 3 minutes running at 1.79, 2.01, 2.24,
230 2.46, 2.68, 2.91, 3.13, 3.35 m/s in randomized order of both speed and gait mode. Each trial was
231 separated by at least 2 minutes rest to avoid fatigue development influencing the performance of
232 the participants. During the walking trials, the participants were instructed to continue to
233 maintain a walk whereby at no point should both feet be off the ground, although the higher

234 speeds might result in discomfort and the urge to start light jog or run. Maintenance of ground
235 contact with at least one foot at all times was visually confirmed. In case of doubt, vertical
236 ground reaction forces recorded by the treadmill-embedded force platforms were consulted (data
237 not included in the study). During running trials, the participants were instructed to continue to
238 maintain a run whereby at no point should both feet be on the ground and there should be a
239 period where both feet were off the ground, although the lower speeds might result in discomfort
240 and the urge to start walking. During all trials, three-dimensional position data of the 15 markers
241 was continuously recorded at 120 Hz using a 12 high-speed camera system (Motion Analysis
242 Corp., Santa Rosa, CA). All subsequent analyses were on kinematic data and the sampling
243 frequency was determined to provide sufficient resolution for toe off event detection, the center
244 of mass displacement, segment and joint angles.

245 **2.3 Data analysis**

246 All analyses were performed using custom written scripts in Matlab (Mathworks 2011, Inc.,
247 Natick, MA).

248 **2.3.1 Continuous relative phase**

249 The marker position data was low pass filtered at 8 Hz with a zero-phase lag, fourth order
250 Butterworth filter. Thigh, shank and foot segment angles with respect to the horizontal line in the
251 sagittal plane of the segment were calculated from each trial (Vaughan et al., 1992). An abrupt
252 change in the anterior-posterior (AP) displacement of the right toe marker indicating the change
253 from a backward to a forward motion during the contact phase was identified as toe off of the
254 right foot. Seventy-five strides (i.e. right toe off to the subsequent right toe off) were identified as
255 the minimum number of completed strides across all strides and all subjects. The AP,
256 mediolateral (ML) and vertical (Vert) displacements, of the sacrum marker were used as a
257 surrogate of the center of mass displacement and were extracted together with the right hip, knee
258 and ankle joint angles for further analysis.

259 The procedure to calculate continuous relative phase is described briefly in the following
260 text but further detail can be found elsewhere (Hamill et al., 1999; Kurz and Stergiou, 2004;
261 Lamoth et al., 2002). It consisted of four steps. First, each segment angle was time-normalized to
262 the stride phase. Second, a phase plane for each segment was created by plotting the normalized
263 segment velocity as a function of the normalized segment angle following the normalization
264 procedure presented by Hamill et al. (1999). Third, the phase angle was calculated as the angle

265 between the right horizontal and the vector connecting two consecutive pairs of coordinates in
266 each of the four quadrants. Phase angles were calculated for the thigh and shank segment
267 flexion/extension and for foot plantar-/dorsiflexion. Finally, the continuous relative phase was
268 calculated for the thigh-shank segment coupling and the thigh-foot segment coupling by
269 subtracting the phase angle of the proximal segment from the phase angle of the distal segment.
270 Continuous relative phase values close to 0° indicate in-phase segment coordination and
271 continuous relative phase values close to 180° indicate out-of-phase segment coordination. The
272 average continuous relative phase for each subject was calculated by averaging it at each time
273 point across the seventy-five strides, and deviation phase was calculated as the standard
274 deviation at each time point across all strides. Finally, the mean continuous relative phase and
275 mean deviation phase were calculated by averaging the continuous relative phase and deviation
276 phase across the stride cycle, respectively.

277 **2.3.2 The largest Lyapunov exponent and correlation dimension**

278 The marker position data was not filtered prior to inclusion in the following analyses.
279 Hip, knee and ankle joint angles in the sagittal plane were calculated (Vaughan et al., 1992) for
280 each trial. Before calculating LyE and CoD, the joint angles and sacrum position time series
281 were reconstructed in state space using the method of delay embedding (Sauer and Yorke, 1993;
282 Sauer et al., 1991; Takens, 1981). The time delay (Tau) was calculated using the Average Mutual
283 Information algorithm and the embedding dimension (EmD) was calculated using the False
284 Nearest Neighbor algorithm (Wurdeman, 2016). In agreement with our previous study (Raffalt et
285 al., 2019), the individual Tau and EmD for each variable and each trial were used to reconstruct
286 each time series in state space. LyE was calculated using the algorithm presented by Wolf et al.
287 (1985) and the CoD was calculated using the algorithm presented by Grassberger and Procaccia
288 (1983).

289 The center of mass displacement variability (i.e. extracted from the sacrum marker
290 position) and joint angle variability were calculated by 1) time-normalizing the time series to
291 100% of each stride, 2) calculating the standard deviation across all strides for each time point
292 and 3) averaging the standard deviation across all time points (meanSD) (James, 2004).

293 **2.4 Statistics**

294 Based on previous studies with similar, research question, experimental design and
295 measures (Diedrich and Warren, 1995; Raffalt et al., 2017), it was estimated that a minimum of

296 10 participants were required to reach significant between-speed and between-gait mode
297 differences of at least 10 % with a statistical power of 80 % and a significance level of 5 %. Due
298 to the inability of a few subjects to walk at the highest speeds and to technical issues, data was
299 lost from 10 out of the total 176 trials (11 subjects x 8 speeds x 2 gait modes). To evaluate the
300 first hypothesis, the effect of speed on each dependent variable was assessed for both gait modes
301 using a mixed model ANOVA for repeated measures with speed as the repeated factor. In case of
302 an overall effect of speed, a Holm-Sidak post hoc test was applied and a quadratic regression
303 analysis was performed to determine the nature of the relationship between speed and the
304 dependent variable in question. The overall percentage of variance accounted for by the
305 regression (r^2) and the p-value were determined. To evaluate the second hypothesis, the effect of
306 speed and gait mode on the dependent variables extracted from the four shared speeds (1.79,
307 2.01, 2.24 and 2.46 m/s) was assessed using a mixed model ANOVA with speed and gait mode
308 as the repeated factors. In case of an overall effect of speed, gait mode and the speed-mode
309 interaction, a Holm-Sidak post hoc test was applied. The level of significance was set at 0.05. All
310 statistics were computed in SPSS (IBM SPSS Statistics, version 24, 2016, USA).

311 **3. Results**

312 **3.1 Segment coordination and coordination variability**

313 There was a significant effect of speed during both walking and running on the mean
314 average continuous relative phase for the thigh-shank segment coupling (Table 1). At relatively
315 low and high walking speeds, the thigh-shank coupling was more out-of-phase compared to the
316 intermediate speeds (Figure 1A). At low running speeds, the coupling was more out-of-phase
317 compared to higher running speeds. For both tasks, there was a significant curvilinear
318 relationship between speed and the relative phase. For the four shared speeds, the segment
319 coordination was more in-phase during walking compared to running. There was a significant
320 effect of speed during both tasks on the mean average continuous relative phase for the thigh-
321 foot segment coupling (Figure 1B). For both tasks, the segment coupling changed in a curvilinear
322 fashion towards more in-phase coordination as speed increased.

323 The coordination variability, assessed by the mean deviation phase, showed similar
324 pattern for both the thigh-shank and thigh-foot segment coupling (Figure 1C and 1D). There was
325 a significant curvilinear relationship between speed and both couplings during the two tasks.
326 During walking, the relationship was U-shaped with the lowest mean deviation phase occurring
327 at the intermediate speeds. During running, the mean deviation phase decreased with increasing
328 speed. There was a significant gait mode-speed interaction in the two-way ANOVA (Table 2),
329 and the post hoc test revealed that the mean deviation phase was higher during running at low
330 speeds and lower during the highest speed when compared to walking.

331 **3.2 Joint angles**

332 There was a significant effect of speed on LyE for the hip and knee joints during walking
333 and for all three joints during running (Table 1). During walking, there was a significant, U-
334 shaped relationship between speed and hip and knee joint LyE with significantly lower values at
335 the intermediate speed of 1.56m/s compared to the lowest and the two highest speeds. During
336 running, the LyE of all three joints decreased significantly in a curvilinear fashion with
337 increasing speed (Figure 2A, 2B and 2C). The two-way ANOVA showed a significant gait
338 mode-speed interaction (Table 2) for all three joints. The post hoc test revealed that the LyE of
339 the hip joint was significantly higher at the two lowest speeds and significantly lower at the
340 highest speed during running compared to walking (Figure 2A). For the knee joint, the LyE of
341 running was significantly higher at the lowest speed and lower at the two highest speeds

342 compared to walking (Figure 2B). For the ankle joint, the LyE during running was significantly
343 lower at the highest speed compared to walking (Figure 2C).

344 There was a significant effect of speed on CoD for all three joints during both tasks
345 (Table 1), with significant curvilinear relationships with speed that resembled those of the LyE.
346 The hip and knee joint CoD exhibited U-shaped relationships with speed during walking and
347 decreasing CoD values with increasing speed during running. For the ankle joint, the CoD
348 decreased with speed during both tasks (Figure 2D, 2E and 2F). There was a significant gait
349 mode-speed interaction for the CoD of the knee joint (Table 2). The post hoc test showed that the
350 CoD was significantly higher during walking at the two highest speeds compared to running
351 (Figure 2E).

352 There was a significant effect of speed on the meanSD for all three joints during both
353 tasks (Table 1). However, only during walking did the meanSD exhibit a significantly curvilinear
354 relationship with speed (Figure 2G, 2H and 2I). For all three joints, the meanSD was
355 significantly higher during the highest walking speed compared to the lower speed. There was a
356 significant gait mode-speed interaction for the meanSD of all three joints (Table 2). For the hip
357 joint, the meanSD was significantly higher during running at the two lowest speeds and
358 significantly lower at the two highest speeds compared to walking (Figure 2G). For the knee and
359 ankle joint, the meanSD was significantly higher during running at the two lowest speeds and
360 significantly lower at the highest speed compared to walking (Figure 2H and 2I).

361 **3.3 Center of mass displacements**

362 There was a significant effect of speed on the LyE of the ML and Vert center of mass
363 displacements during walking (Table 1). While the LyE increased curvilinearly with speed in the
364 ML direction, no between-speed differences were observed in the Vert direction (Figure 3B and
365 3C). There was a significant gait mode-speed interaction in the ML direction (Table 2) and the
366 post hoc test revealed that the LyE during walking at the highest speed was significantly higher
367 compared to running (Figure 3B).

368 There was a significant effect of speed on the center of mass CoD in the ML and Vert
369 directions during walking (Table 1). In both cases, a U-shaped relationship was observed with
370 significantly lower CoD at the intermediate speeds compared to the two highest speeds (Figure
371 3E and 3F). For the ML and Vert directions, there was a significant gait mode-speed interaction
372 (Table 2). In the ML direction, the CoD was significantly higher at the two lowest speeds during

373 running compared to walking (Figure 3E) and in the Vert direction, the CoD was significantly
374 higher at all four speeds during walking compared to running (Figure 3F).

375 There was a significant effect of speed on the meanSD of the center of mass
376 displacements in the Vert direction during walking and the AP and Vert direction during running
377 (Table 1). In the AP direction during running, the meanSD decreased curvilinear with increasing
378 speed (Figure 3G) and in the Vert direction, the meanSD increased significantly at the two
379 highest walking speed (Figure 3I). There was no significant curvilinear relationship for the Vert
380 center of mass displacement during running. There was a significant gait mode-speed interaction
381 in the Vert direction (Table 2) and the meanSD was significantly higher at the two lowest speeds
382 and higher at the highest speed during running compared to walking (Figure 3I).

383

384 4. Discussion

385 The work by Diedrich and Warren (Diedrich and Warren, 1998; Diedrich and Warren,
386 1995) laid the theoretical foundation for understanding the mechanisms governing the walk-to-
387 run transition in humans from a Dynamical Systems Theory perspective. Based on their studies,
388 two principles can be inferred: the *control parameter-dependent attractor stability principle*,
389 which suggests that changing locomotion speed above and below the preferred speed of a given
390 gait mode would move the system from a stable attractor to regions of instability, and the
391 *attractor stability optimization principle*, which suggests the self-selected gait mode at a given
392 speed would exhibit a more stable attractor compared to the alternative non-self-selected gait
393 mode. However, the work by Diedrich and Warren (Diedrich and Warren, 1998; Diedrich and
394 Warren, 1995) was limited by only quantifying the spatial variation in the coordination of
395 segmental motion using relative phase and did not include an assessment of the temporal
396 dynamics of relevant variables. Therefore, the purpose of the present study was to investigate the
397 attractor stability of walking and running across a range of speeds when both stable self-selected
398 movement solutions and unstable non-self-selected movement solutions were evoked. The
399 present study adopted the methodological and analytical approach used by Diedrich and Warren
400 (1995) by quantifying the stability of the executed lower limb coordination pattern using
401 deviation phase. In addition, the present study quantified the temporal dynamics and movement
402 variability of the lower limb joint angles and the center of mass displacement. In agreement with
403 the inferred principles, it was hypothesized that 1) the movement solution during walking at
404 PWS and during running at PRS is a stable behavioral attractors for that particular gait mode
405 while speeds below and above would display significantly different dynamics and 2) at speeds
406 close to the preferred speed of a particular gait mode the movement solution would exhibit more
407 stable attractor behavior compared the alternative gait mode. Additionally, the present study
408 sought to clarify whether a center of mass movement-based or a lower limb joint angle-based
409 attractor behavior constitutes the most appropriate order parameter for human locomotion.

410 4.1 Control parameter dependent attractor stability principle

411 The first hypothesis related to the *control parameter-dependent attractor stability*
412 *principle* was partially supported. Clear U-shaped relationships with local minima close to the
413 PWS were observed across walking speeds in the mean deviation phase for both the thigh-shank
414 and thigh-foot segment couplings (see Figure 1C and D), the LyE and CoD for the hip and knee

415 joint angle (see Figure 2A, B, D and E), and the meanSD for all three joint angles (see Figure 2G
416 and H). This suggests that the first inferred principle holds true during walking when assessing
417 lower limb coordination stability, when assessing the lower limb temporal dynamics for the hip
418 and knee joint and when assessing movement variability of all three lower limb joints. It is
419 noteworthy that the local minima for the variables in question tended to lie at a speed slightly
420 above the PWS. This specific phenomenon has also been observed in previous studies focusing
421 on the effect of walking speed on the temporal dynamics of lower limb joint angles and stride
422 characteristics (Chien et al., 2015; Jordan et al., 2007; Raffalt et al., 2017). However, it has not
423 been addressed by the previous studies. It could indicate that the PWS is actually an
424 underestimation of the optimal speed for the body and task during walking. This could either be
425 a methodological issue with the PWS assessment, an artifact of altered walking due to the
426 treadmill, or suggest that the PWS is influenced by physiological and psychological aspects
427 unrelated to movement coordination. Interestingly, the results of the present study did not seem
428 to support the application of the *control parameter-dependent attractor stability principle* to
429 running. For the coordination stability and for the hip and knee joint angle dynamics, there was a
430 clear pattern of increasing attractor stability as running speed increased beyond the preferred
431 running speed; the deviation phase of the thigh-shank segment and thigh-foot segment couplings
432 decreased with increased running speed, as did both LyE and CoD. This suggests that the factors
433 determining the preferred running speed are not related to the factors determining the attractor
434 stability of running. This apparent difference between walking and running could be explained
435 by the functional role of the lower limb during the two tasks.

436 During the contact phase of walking, the lower limb functions as an inverted pendulum
437 that moves the center of mass forward across the area of support with a continuous exchange of
438 potential and kinetic energy (Cavagna and Margaria, 1966; Cavagna et al., 1963). Furthermore,
439 during the swing phase, the lower limb functions as double pendulum. Accordingly, the leg
440 swing frequency (i.e. equivalent to the step frequency) at the preferred walking speed equals the
441 resonant frequency of the system, which coincides with a maximal knee joint stability (Russell
442 and Haworth, 2014) and the minimum muscle activity and energy expenditure (Holt et al., 1995;
443 Russell and Apatoczky, 2016). The swinging motion of a pendulum depends on its length,
444 which, in the case of human walking, changes minimally in comparison to overall leg length.
445 This suggests that the self-organization process during walking would seemingly need to adjust

446 for minimal scaling changes in the mechanical properties of the lower limb as compared to more
447 substantial changes in swinging frequency consequential of altered gait speed. Thus, the optimal
448 attractor stability during walking is closely linked to the resonant frequency of the lower limb. In
449 contrast, during the contact phase of running the lower limb functions as a mechanical spring, in
450 which elastic energy is stored during the initial braking phase and then released during the later
451 propulsion phase (Blickhan, 1989). The efficiency of a spring relates to its stiffness, and it has
452 been shown that leg stiffness is linearly proportional to both running speed and stride frequency
453 (Arampatzis et al., 1999; Farley and González, 1996). The stiffness of the limb is increased by
454 increasing muscle activity surrounding the lower limb joints with the purpose of efficiently
455 utilizing elastic energy (Hobara et al., 2007; Moritani et al., 1991). When analyzing hopping, it
456 has been suggested that as hopping frequency increases, the leg stiffness is increased by greater
457 preactivation of the triceps surae prior to ground contact. This occurs in conjunction with an
458 altered short-latency stretch reflex response (Hobara et al., 2007; Voigt et al., 1998). Similar
459 changes in reflex and EMG responses have been observed during running with increasing speeds
460 (Simonsen et al., 2012), when the stride frequency increases and contact time decreases,
461 simultaneously. This would suggest that the control mechanism for increasing the leg stiffness
462 simplifies, making the entire spring system simpler with fewer degrees of freedom. Simplifying
463 one or more components in the self-organization process may permit greater attractor stability.
464 Furthermore, during running the forward swinging motion of the leg requires a higher high
465 angular velocity than can be created alone by the pendulum motion caused by gravity. Therefore,
466 considerable muscle activity in hip flexor muscles is required to generate the needed torque
467 (Modica and Kram, 2005). Thus, due to this speed-related change in mechanical properties and
468 control mechanisms of the spring components and the added torque to the pendulum motion, it
469 may be unfeasible to reach an optimum in attractor stability during running at the speeds used in
470 the present study.

471 It is noteworthy that the highest running speed of the present study was 3.35 m/s (equal to
472 12.1 km/h or 7.5 mph). This is well below what many healthy individuals are capable of running
473 at and it is possible that the attractor stability would eventually decrease if higher running speeds
474 were tested. If that was the case, it would provide evidence to confirm the *control parameter-*
475 *dependent attractor stability principle* for running as well. However, testing this would have, for
476 safety reasons, required more experienced treadmill runners. Furthermore, running and sprinting

477 at very high speeds will alter the foot strike pattern for most individuals from a heel strike pattern
478 to a forefoot strike pattern. It is possible that a change in foot strike pattern with increasing speed
479 would affect the self-organization process of the system and significantly change the attractor
480 stability. However, it is beyond the scope of this study to elucidate this aspect.

481 **4.2 Attractor stability optimization principle**

482 The second hypothesis related to the *attractor stability optimization principle* stated that
483 the movement solution would exhibit more stable attractor behavior at speeds close to the
484 preferred speed of that particular gait mode compared to the alternative gait mode. A more stable
485 attractor behavior would be characterized by a low deviation phase when using the relative phase
486 approach, by a coinciding low LyE and CoD when assessing the dynamics of the attractor
487 behavior, and by a low meanSD when assessing movement variability. This hypothesis was
488 supported for the relative phase approach, for the dynamics of the attractor behavior of the hip
489 and knee joint angles, and for the movement variability of all three joints but not for the center of
490 mass displacement. First, a lower deviation phase for both joint couplings (see Figure 1C and D),
491 and a lower LyE and lower movement variability for the hip and knee joint angles (see Figure
492 2A, B, G and H) were observed during walking compared to running at 1.79m/s. Second, at
493 2.46m/s running elicited a lower deviation phase for both joint couplings, a lower LyE and lower
494 movement variability for the hip and knee joint angles compared to walking.

495 The results for attractor stability when assessed with deviation phase verify the results
496 presented by Diedrich and Warren (1995), and show that the attractor stability was highest at a
497 particular gait mode at speeds closest to the corresponding mode's preferred speed. This was true
498 for both the thigh-shank segment and thigh-foot segment couplings. While this supports the
499 *attractor stability optimization principle*, the applied methodology does not take into account the
500 temporal dynamics of the system. Thus, it is crucial to also evaluate the principle in question
501 through an assessment of the temporal dynamics of the attractor behavior. This was achieved in
502 the present study by quantifying the LyE and CoD of the hip, knee and ankle joint angles and the
503 center of mass displacement. It was evident that the principle also holds true for the dynamics of
504 the hip and knee joint angles and to a lesser extent for the ankle joint angle. This phenomenon
505 was not observed for the center of mass displacements. Our results clearly demonstrate that for
506 the hip and knee joint dynamics, the self-selected gait mode at a given speed was characterized
507 by a more stable attractor compared to that of the alternative non-self-selected gait mode. In

508 relation to the functional role of the lower limb and the self-organization process, this indicates
509 that forcing the leg to function as a spring (i.e. running) is inexpedient when the constraints of
510 the tasks (relatively low speed) favor an inverted pendulum function (i.e. walking) to create a
511 stable attractor behavior. Equally, forcing an inverted pendulum function when the tasks
512 constraints favor a spring function seems inexpedient at relatively high speeds. The results of the
513 present study suggest that the hip and knee joint angles and the corresponding oscillatory motion
514 of the thigh and shank segment are better determining for the limb function than the ankle joint
515 and foot segment motion. When quantifying the attractor stability through the movement
516 variability of the joint angles, the principle was also confirmed. Thus, the movement variability
517 was observed to be lower at a given speed when using the self-selected gait mode. However,
518 assessing movement variability via meanSD suffers from the same limitation as the relative
519 phase approach by not incorporating the temporal dynamics which is a key element of any
520 nonlinear dynamical system (Stergiou, 2004; Stergiou, 2016).

521 The walk-to-run transition speed and the run-to-walk transition speed (neither measured
522 in the present study) are expected to lie somewhere between the PWS and the PRS. In the present
523 study, both walking and running were performed at four different speeds between the PWS and
524 PRS. The attractor stability for one gait mode increased beyond the stability for the alternative
525 mode within these four speeds, indicating that the gait mode transition lies between these four
526 speeds. Furthermore, for one or both of the two intermediate speeds (2.01 and 2.24m/s), the
527 attractor stability was nearly the same, suggesting that neither of the two gait modes
528 outperformed the other. However, when the speed is either decreased or increased slightly to
529 either 1.79 or 2.46, a clear favorable movement solution was available. In support of the notion
530 presented by Diedrich and Warren (1995), the present study suggests that the choice to walk or
531 run at a given speed is determined by whatever gait mode provides the highest lower limb
532 attractor stability.

533 **4.3 Human locomotion order parameter**

534 The present study had a secondary purpose of identifying an appropriate order parameter
535 for walking and running. No clear consensus exists in the literature and various variables related
536 to the center of mass or the lower limb motions have been used (Diedrich and Warren, 1995;
537 Dingwell and Marin, 2006; England and Granata, 2007; Kurz et al., 2005; Raffalt et al., 2017;
538 Stergiou et al., 2001). In the present study, it was speculated that the variable(s) supporting the

539 raised hypotheses would be the most appropriate order parameter(s) for capturing the system
540 dynamics during locomotion. Our results suggest that variables that incorporated the lower limb
541 motions are superior in describing the attractor behavior of the system, compared to variables
542 based on the center of mass displacement. In particular, the deviation phase, which describes the
543 stability of the oscillatory segment coupling, and the LyE and CoD, which describe the temporal
544 dynamics of the hip and knee joint angles, seemed to clearly capture the changes in attractor
545 behavior as speed was increased or movement task was changed.

546 Notably, the temporal dynamics and the movement variability of the center of mass
547 displacements did not support the two inferred principles, and no consistent pattern could be
548 observed across the three directions as speed or movement task were changed (see Figure 3).
549 These observations question the use of center of mass movements when evaluating the system's
550 attractor behavior during locomotion. Previously, quantifying LyE of center of mass movements
551 has been linked to the overall stability of gait and the risk of falling (Bruijn et al., 2012; Bruijn et
552 al., 2013). However, very different results have been reported in the literature when assessing
553 LyE on the center of mass movements during walking at different speeds (Bruijn et al., 2009;
554 Dingwell and Marin, 2006; Raffalt et al., 2017). While this potentially may be due to different
555 methodological approaches (Raffalt et al., 2019; Stenum et al., 2014), based on the results of the
556 present study, caution should be exercised when using the center of mass motion as an order
557 parameter for human locomotion.

558 While not appropriate as an order parameter for human locomotion when addressing
559 attractor behavior, the vertical center of mass displacement in particular seems closely related to
560 the energetics of walking (Gottschall and Kram, 2003; Grabowski, 2010; Wurdeman et al.,
561 2017). Thus, the dynamics and movement variability of the vertical center of mass displacement
562 in the present study best resembled the U-shaped relationship between oxygen uptake and
563 walking speed previously observed (Raffalt et al., 2017; Ralston, 1958; Zarrugh et al., 1974).

564 **4.4 Study limitation**

565 The present study used absolute speeds similar to the study by Bruijn et al. (2009). This is
566 in contrast to studies that have used either Froude number-based speeds (Diedrich and Warren,
567 1998; Diedrich and Warren, 1995; England and Granata, 2007; Raffalt et al., 2017) or relative
568 PWS (Chien et al., 2015; Dingwell and Marin, 2006). There are pros and cons for each approach;

569 however, when designing this protocol we prioritized the inclusion of four speeds at which all
570 participants were able to both walk and run.

571 The method of identifying PWS and PRS was adopted from Dingwell and Marin (2006)
572 who used it only to find PWS. While there is no reason to believe that the method is
573 inappropriate for running, it is possible that the method is less effective when applied to running.
574 This may further explain differences in the observations for running compared to walking in the
575 present study. The PRS observed in the present study was relatively low compared to preferred
576 speeds that might be expected in competitive runners. Thus, the results of the present study
577 cannot be extrapolated to individuals with substantial running experience.

578

579 **5. Conclusion**

580 In conclusion, the present study showed that lower limb attractor stability during walking
581 is maximized at speeds close to PWS. For running, however, lower limb attractor stability
582 increases as running speed is increased beyond PRS. Furthermore, the present study showed that
583 the attractor stability is highest at a particular gait mode closest to the corresponding preferred
584 speed. These results provide confirmation of the observations made by Diedrich and Warren
585 (Diedrich and Warren, 1998; 1995) and support the *control parameter-dependent attractor*
586 *stability principle* and the *attractor stability optimization principle* inferred from their studies.
587 Finally, the present study suggests that the dynamics and relative phase of lower limb motion
588 provide a more appropriate order parameter for quantifying attractor behavior during human
589 locomotion compared to the dynamics of center of mass displacement.

590

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594

595 **Competing interests**

596 No competing interests declared.

597

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601

602 **Legends**

603 **Table 1: Effect of speed during walking and running.** Results of the one-way mixed
604 model ANOVA for repeated measures with speed as the independent factor ($n=11$).

605
606 **Table 2: Effect of gait mode and speed on attractor behavior stability.** Results of the
607 two-way mixed model ANOVA for repeated measures with gait mode and speed as independent
608 factors and the mode-speed interaction ($n=11$).

609
610 **Fig 1: Mean average continuous relative phase and mean deviation phase.** Group
611 ($n=11$) mean \pm s.e.m. of the mean average continuous relative phase and mean deviation phase for
612 the thigh-shank and thigh-foot segment coupling during walking and running. In the case of a
613 significant effect of speed (mixed model ANOVA for repeated measures, $p < 0.005$) and a
614 significant curvilinear relationship, a regression line is added. Grey areas indicate the mean \pm
615 standard deviation of PWS and PRS. * indicates significant difference in the dependent variable
616 between gait modes (mixed model ANOVA, $p < 0.005$).

617
618 **Fig 2: The largest Lyapunov exponent, correlation dimension, movement variability**
619 **of the hip, knee and ankle joint angle.** Group ($n=11$) mean \pm s.e.m. of the LyE, CoD and
620 meanSD for the hip, knee and ankle joint angle during walking and running. In the case of a
621 significant effect of speed (mixed model ANOVA for repeated measures, $p < 0.005$) and a
622 significant curvilinear relationship, a regression line is added. Grey areas indicate the mean \pm
623 standard deviation of PWS and PRS. * indicates significant difference in the dependent variable
624 between gait modes (mixed model ANOVA, $p < 0.005$).

625
626 **Fig 3: The largest Lyapunov exponent, correlation dimension, movement variability**
627 **of the center of mass displacement.** Group ($n=11$) mean \pm s.e.m. of the LyE, CoD and meanSD
628 for the center of mass displacement in the anterior-posterior, mediolateral and vertical direction
629 during walking and running. In the case of a significant effect of speed (mixed model ANOVA
630 for repeated measures, $p < 0.005$) and a significant curvilinear relationship, a regression line is
631 added. Grey areas indicate the mean \pm standard deviation of PWS and PRS. * indicates

632 significant difference in the dependent variable between gait modes (mixed model ANOVA, $p <$
633 0.005).
634

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787 **Table 1: Effect of speed on attractor behavior stability during walking and running.**
788 Results of the one-way mixed model ANOVA for repeated measures with speed as the
789 independent factor.

		Walking		Running	
		F-value	p-value	F-value	p-value
Continuous relative phase	Thigh-shank	5.13	< 0.0001	8.81	< 0.0001
	Thigh-foot	92.87	< 0.0001	7.95	< 0.0001
Deviation phase	Thigh-shank	11.09	< 0.0001	26.91	< 0.0001
	Thigh-foot	16.58	< 0.0001	39.04	< 0.0001
Lyapunov exponent	Hip joint	14.13	< 0.0001	13.34	< 0.0001
	Knee joint	18.60	< 0.0001	3.64	0.002
	Ankle joint	2.02	NS	2.69	0.015
Correlation dimension	Hip joint	8.02	< 0.0001	6.34	< 0.0001
	Knee joint	13.10	< 0.0001	9.98	< 0.0001
	Ankle joint	3.24	0.005	6.78	< 0.0001
Movement variability	Hip joint	26.21	< 0.0001	3.41	0.003
	Knee joint	17.96	< 0.0001	3.81	0.001
	Ankle joint	14.67	< 0.0001	2.91	0.010
Lyapunov exponent	Ant-Pos	1.855	NS	1.62	NS
	Med-Lat	20.18	< 0.0001	1.19	NS
	Vert	2.42	0.028	0.884	NS
Correlation dimension	Ant-Pos	0.83	NS	1.61	NS
	Med-Lat	5.19	< 0.0001	1.59	NS
	Vert	4.17	0.001	1.31	NS
Movement variability	Ant-Pos	1.48	NS	2.94	0.009
	Med-Lat	1.47	NS	1.42	NS
	Vert	21.18	< 0.0001	3.79	0.001

790 NS: not significant

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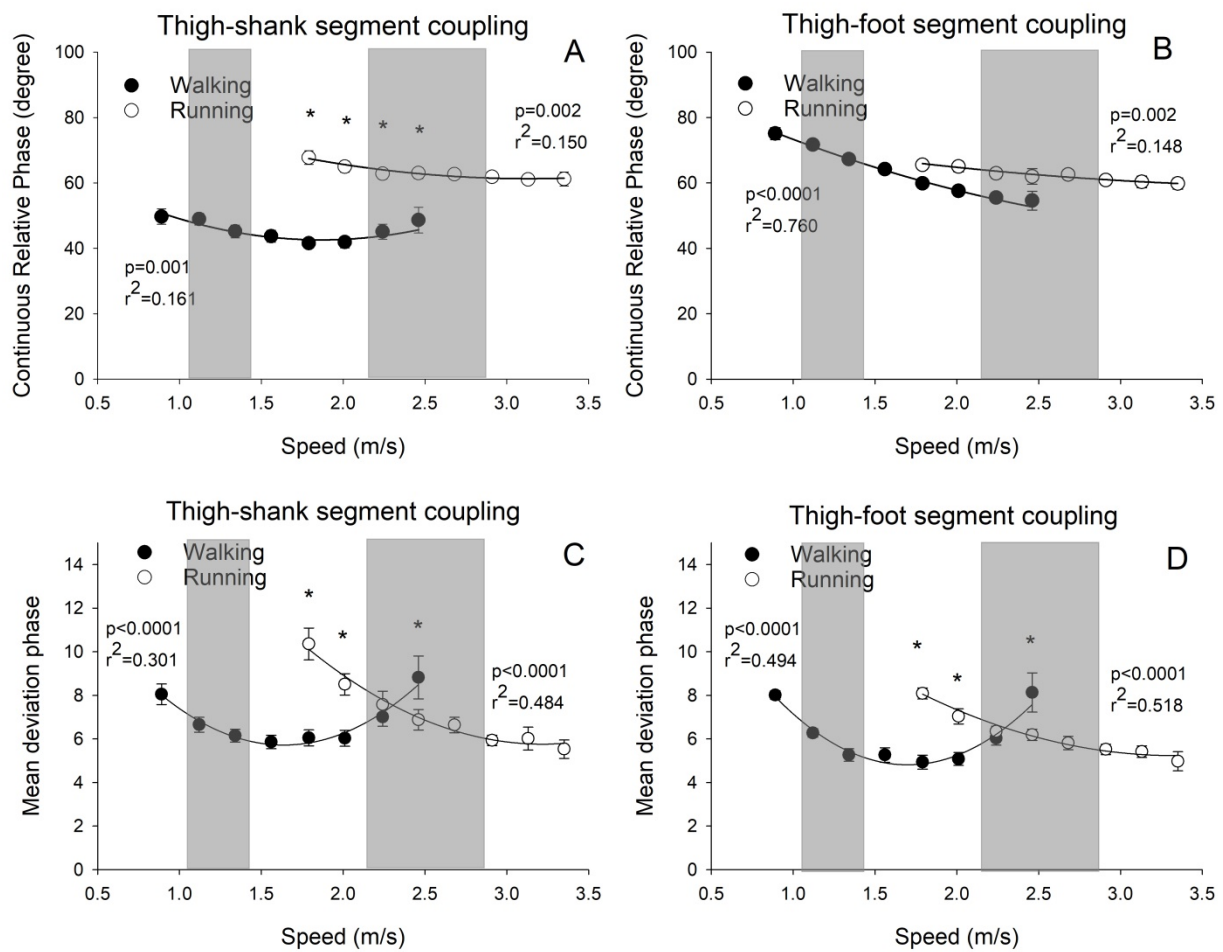
792 **Table 2: Effect of gait mode and speed on attractor behavior stability.** Results of the
793 two-way mixed model ANOVA for repeated measures with gait mode and speed as independent
794 factors and the mode-speed interaction.

		Gait mode		Speed		Mode-speed interaction	
		F-value	p-value	F-value	p-value	F-value	p-value
Continuous relative phase	Thigh-shank	485.7	< 0.0001	0.64	NS	5.43	0.002
	Thigh-foot	98.01	< 0.0001	8.56	< 0.0001	0.57	NS
Deviation phase	Thigh-shank	40.84	< 0.0001	4.89	0.004	34.64	< 0.0001
	Thigh-foot	24.56	< 0.0001	2.82	0.045	28.92	< 0.0001
Lyapunov exponent	Hip joint	23.07	< 0.0001	0.80	NS	18.33	< 0.0001
	Knee joint	15.79	< 0.0001	5.75	0.001	12.77	< 0.0001
	Ankle joint	4.77	0.032	0.24	NS	2.87	0.043
Correlation dimension	Hip joint	0.12	NS	2.04	NS	1.39	NS
	Knee joint	13.21	0.001	1.20	NS	4.90	0.004
	Ankle joint	1.66	NS	3.59	0.018	2.02	NS
Movement variability	Hip joint	0.36	NS	11.97	< 0.0001	36.32	< 0.0001
	Knee joint	0.001	NS	10.59	< 0.0001	22.72	< 0.0001
	Ankle joint	6.55	0.013	7.97	< 0.0001	21.79	< 0.0001
Lyapunov exponent	Ant-Pos	0.16	NS	0.80	NS	1.03	NS
	Med-Lat	1.80	NS	8.19	< 0.0001	8.25	< 0.0001
	Vert	11.37	0.001	0.82	NS	1.58	NS
Correlation dimension	Ant-Pos	17.09	< 0.0001	0.89	NS	0.63	NS
	Med-Lat	23.64	< 0.0001	4.47	0.006	4.76	0.004
	Vert	73.54	< 0.0001	2.26	NS	3.22	0.028
Movement variability	Ant-Pos	0.50	NS	1.07	NS	1.67	NS
	Med-Lat	0.97	NS	1.57	NS	0.60	NS
	Vert	10.89	0.002	10.35	< 0.0001	22.19	< 0.0001

795 NS: not significant

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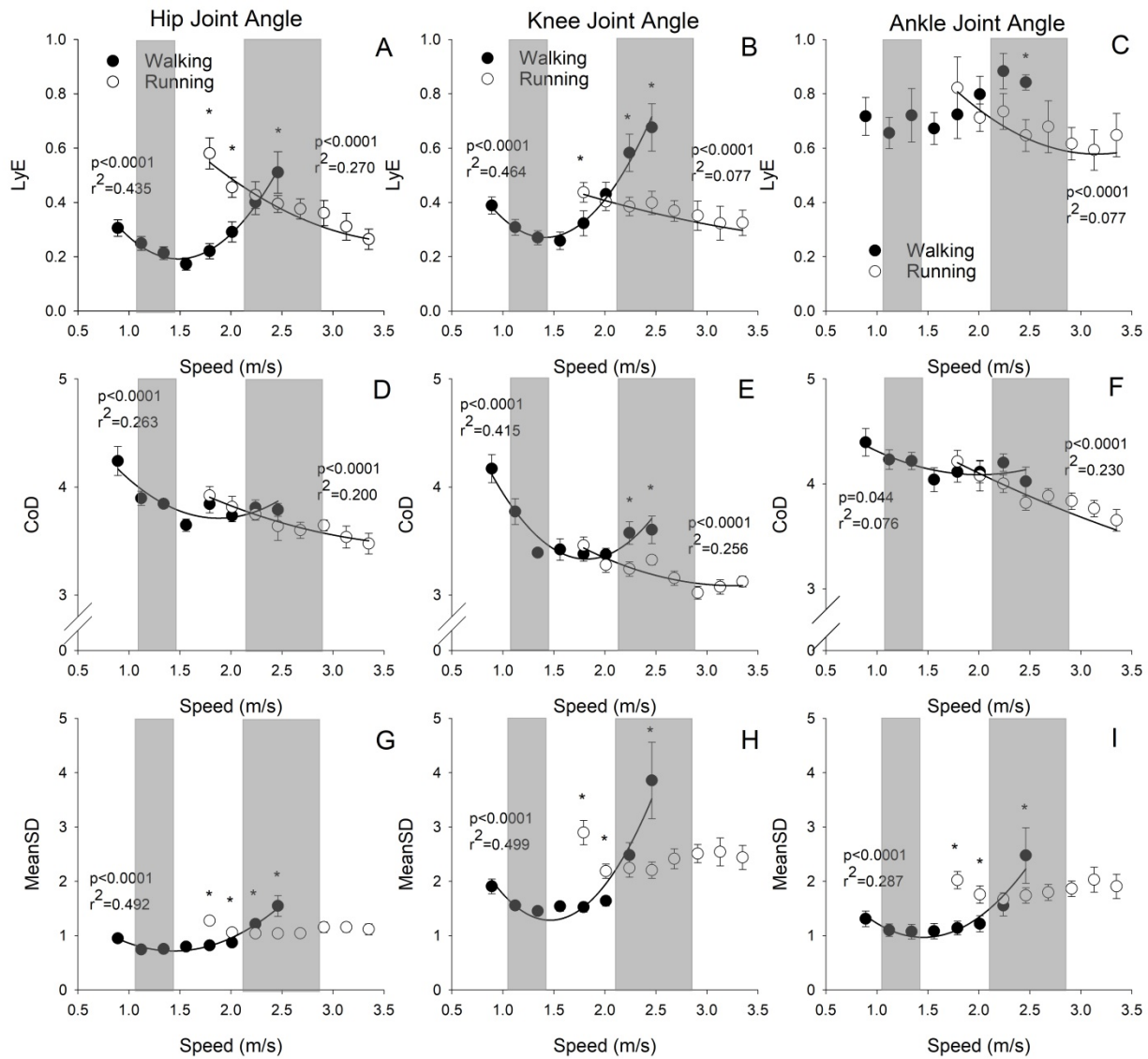
797 **Fig 1: Mean average continuous relative phase and mean deviation phase.** Group
 798 ($n=11$) mean \pm s.e.m. of the mean average continuous relative phase and mean deviation phase for
 799 the thigh-shank and thigh-foot segment coupling during walking and running. In the case of a
 800 significant effect of speed (mixed model ANOVA for repeated measures, $p < 0.005$) and a
 801 significant curvilinear relationship, a regression line is added. Grey areas indicate the mean \pm
 802 standard deviation of PWS and PRS. * indicates significant difference in the dependent variable
 803 between gait modes (mixed model ANOVA, $p < 0.005$).
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807 **Fig 2: The largest Lyapunov exponent, correlation dimension, movement variability**
 808 **of the hip, knee and ankle joint angle.** Group ($n=11$) mean \pm s.e.m. of the LyE, CoD and
 809 meanSD for the hip, knee and ankle joint angle during walking and running. In the case of a
 810 significant effect of speed (mixed model ANOVA for repeated measures, $p < 0.005$) and a
 811 significant curvilinear relationship, a regression line is added. Grey areas indicate the mean \pm
 812 standard deviation of PWS and PRS. * indicates significant difference in the dependent variable
 813 between gait modes (mixed model ANOVA, $p < 0.005$).

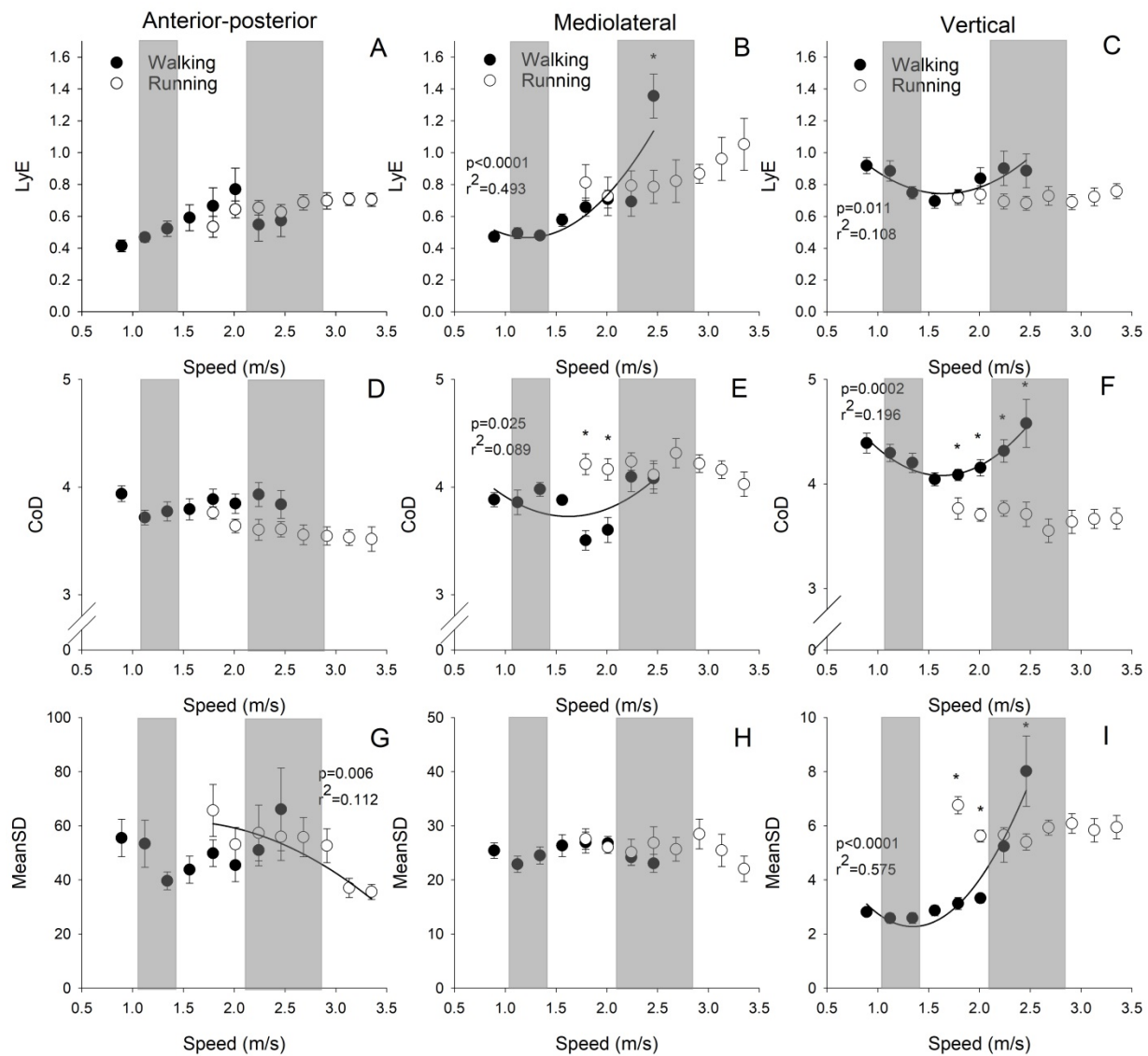
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817 **Fig 3: The largest Lyapunov exponent, correlation dimension, movement variability**
 818 **of the center of mass displacement.** Group ($n=11$) mean \pm s.e.m. of the LyE, CoD and meanSD
 819 for the center of mass displacement in the anterior-posterior, mediolateral and vertical direction
 820 during walking and running. In the case of a significant effect of speed (mixed model ANOVA
 821 for repeated measures, $p < 0.005$) and a significant curvilinear relationship, a regression line is
 822 added. Grey areas indicate the mean \pm standard deviation of PWS and PRS. * indicates
 823 significant difference in the dependent variable between gait modes (mixed model ANOVA, $p <$
 824 0.005).
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